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HEAT INSULATION ANALYSIS OF AN ALUMINIUM HONEYCOMB SANDWICH STRUCTURE

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ABSTRACT

Heat-transfer has been performed on a sandwich thermal protection system (TPS) for future flight vehicles. The sandwich structures are built from thin walled metal sheets. These structures as a part of the airframe outer cover provide thermal protection to the interior parts mounted inside the vehicle. The temperature protection materials used for sandwich structures should have high strength even at the elevated temperatures. It is easier to simulate the 150° C (after 150^o C material properties are changed) temperature on the Aluminium sandwich structures and find the temperature gradient across the sandwich depth. Though the experiment was done on hexagonal cells honeycomb, the ANSYS analyses have been done for both square cell's sandwich panel and hexagonal honeycomb panel for comparison. Experiments are done on using Al alloy honeycomb sandwich panels and the validations of experimental work using ANSYS analysis have been performed. ANSYS modeling, analysis has been done for both, the square and hexagonal honevcomb sandwich panels of the Al alloy. This paper focuses on the heat transfer analysis and in exploring the ways to reduce the heat transfer effect with the methods mentioned above, which could be effectively used for flight vehicle applications.

1. INTRODUCTION

Sandwich panels are used for the design and construction of lightweight transportation systems such as satellites, aircraft, Structural weight saving is the major and missiles. consideration and sandwich construction the is frequently used instead of increasing material thickness, honeycomb is made of very thin material. They reduce the weight, while providing the structural rigidity. This type of sandwich construction consists of two thin facing layers separated by a core material. Potential materials for sandwich facings are aluminium alloys, high tensile steels, titanium, inconel-617 and composites with honeycomb cores and a suitable matrix depending on the specific mission requirement. Several types of core shapes and core materials have been applied to the construction of sandwich structures. Among them, the honeycomb core that consists of very thin foils in the form of hexagonal cells perpendicular to the facings is the most popular.

Honeycomb sandwich structure as shown in Figure 1 are currently being used in the construction of high performance aircraft and missiles and are also being proposed for construction of future high speed vehicles. The design of a vehicle for high speed flight must be supported by structural temperature predictions and the amount of heat transferred through the exterior panels during flight. In order to predict these quantities, it is necessary to have knowledge of the heat transfer characteristics of the honeycomb panel.

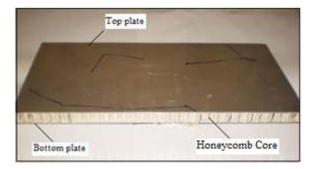


Figure 1 Honeycomb sandwich structure

1.1 Honeycomb Structures

In structural sandwiches, face sheets are mostly identical in material and thickness and they primarily resist the in-plane and bending loads. These structures are called symmetric sandwich structures. However, in some special cases face sheets may vary in thickness or material because of different loading conditions or working environment. This configuration is named as asymmetric sandwich structures. In general sandwich structures are symmetric; the variety of sandwich constructions basically depends on the configuration of the core. The core of a sandwich structure can be almost any material or architecture, but in general they are classified into four types, foam or solid core, web core, corrugated or truss core and honeycomb core, the exploded view of the honeycomb core sandwich structure is shown in Figure 2. The adhesion of face sheets and core is another important criterion for the load transfer and for the functioning of the sandwich structure as a whole.

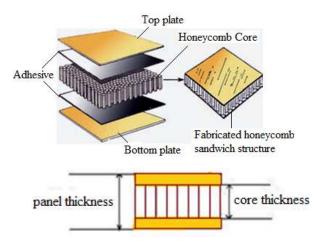


Figure 2 Exploded view of honeycomb core sandwich structure

1.2 Honeycomb Core

The purpose of the core is to increase the flexural stiffness of the panel. The honeycomb core as shown in Figure 3, in general, has low density in order to add as little as possible to the total weight of the sandwich construction. The core must be stiff enough in shear and perpendicular to the faces to ensure that face sheets are at a constant distance apart to prevent their detachment.

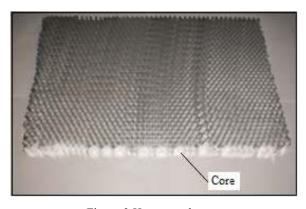


Figure 3 Honeycomb core

1.3 High Temperature Adhesives

High Temperature Adhesives find their application mainly in aerospace industries. A number of adhesives available can operate at high temperatures than epoxies and phenolics. These adhesives are really expensive and require high cure temperatures, and sometimes complicated cure schedules.

1.4 Application Areas of Sandwich Structures

The use of honeycomb sandwich structures in aeronautical and aerospace, applications are getting wider as these structures have excellent stiffness to weight ratios that leads to weight reduction. In aerospace applications various honeycomb cored sandwich structures were used for space shuttle constructions. They are also used for both military and commercial aircraft.

2. NOMENCLATURE

- *L* Length of a Rectangular Plate, mm
- w Width of a Rectangular Plate, mm
- a Depth of the Honeycomb Core, mm
- A Surface area, Square meters
- K Thermal Conductivity, w/m-k
- h Heat transfer Coefficient, w/m²-k
 - Time, sec

t

- c_p Specific Heat, j/kg-k
- T_{∞} Ambient Temperature, °C
- T Temperature to be measured at time (t), °C
- T_i Inner face face sheet temperature, °C
- T_o Outer face face sheet temperature, ^oC

 ΔT Difference between outer and inner face sheet temperature, °C

- tc Honeycomb cell wall thickness ,mm tc
- ts Sandwich face sheet thickness, mm
- b₁ Length of bonded side of hexagonal cell, mm

- d₁ Size of diagonal of hexagonal cell, mm
- b₂ Length of bonded side of square cell, mm
- d₂ Size of diagonal of square cell, mm

3. MATERIAL PROPERTIES

The honeycomb panel material was modelled as a sandwich structure with three layers through the thickness. For Aluminium honeycomb panel (upper & lower parts) material is Al-2024 and core material is Al-3003. These properties are summarized in Table-1.

S.No	Properties	Al-2024	Al-3003
1	Thermal	121	162
	Conductivity		
	$W/(m^{o}C),$		
2	Heat Transfer	25	25
	Coefficient		
	(W/m ² -K)		
3	Poisson ratio	0.33	0.33
4	Density	2780	2730
	(Kg/m ³)		
5	Specific Heat	875	893
	J/(kg K)		
6	Thermal	22.9×10 ⁻⁶	23.1×10 ⁻⁶
	Expansion		
	(m/m-°C)		

4. HONEYCOMB CELL GEOMETRY

Figure 4 shows two types of honeycomb cell geometry to be analyzed. The honeycomb cell wall thickness for the first two types is t(c). The first type is a right, hexagonal cell with identical side lengths of b₁. The second type is a square cell with side lengths of b₂, which is modified from the right, hexagonal cell by reducing the bonding interface length to a minimum of $\sqrt{2} tc$. The size, d(i) (i=1,2) of each type of honeycomb cell is defined as the maximum diagonal of the cell cross section. The size of honeycomb cells types 1, 2, are adjusted to have the same effective density (that is, $\rho_1 = \rho_2$). Honeycomb structures are composed of plates or sheets that form the edges of unit cells.

4.1 Two-dimension model of Honeycomb Sandwich Structure

In this model, the aluminium honeycomb core was 3003 material and upper & lower plates was 2024 materials, with reduced mass density. Otherwise, the general structure of the sandwich material remained the same, with an aluminum core, trapped between two aluminum plates, with adhesive layers between the two species. Temperature independent values were

taken for the conductivity and capacity of the honeycombequivalent material, while the properties of the other materials were the same. Figure 5 is a cartoon representing the 2D model implemented in this paper.

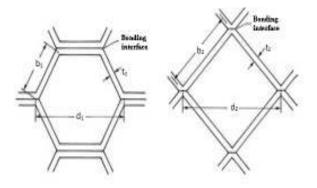


Figure 4 (a) Right hexagonal cell. (b) Square cell

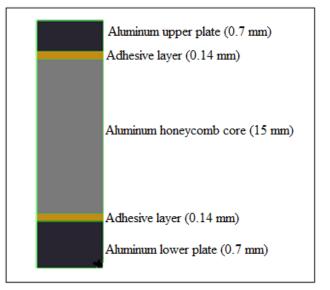


Figure 5 Two-dimensional model of Honeycomb Sandwich Structure

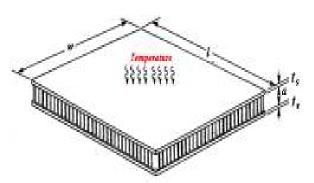


Figure 6 Honeycomb sandwich thermal protection system (TPS) subjected to overheating entire upper surface.

Figure 6 shows a honeycomb-core sandwich thermal protection system panel subjected to transient surface temperature, over its entire outer surface. The thermal protection system panel is rectangular with a side length -l and width-w, and is fabricated with two identical face sheets with a thickness of t_s and honeycomb core with a depth of a. For a given material, the overall heat-insulation performances of the honeycomb thermal protection system panel depend on the thickness of the face sheets, depth of the honeycomb core, thickness of the honeycomb cell walls, and size and shape of the honeycomb cells,

3.2 Numerical Input Values

A typical candidate honeycomb sandwich structures has the following dimensions:

l = 115 mm, w = 85 mm, d₁ = 7 mm, d₂ = 7.42mm, b₁ = 3.5 mm, b₂ = 5.25 mm, t_s = 0.7 mm, a = 15 mm, t_c = 0.005 mm

3.3 Modelling Details

Design is done in ANSYS by Modelling. Type of Mesh is Tet-Free Mesh Size is 0.001 ; Time step is 90 seconds (i.e 1.3 degree C per second)

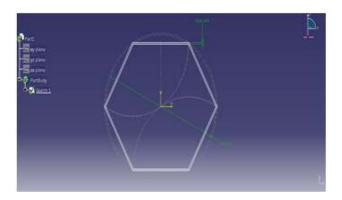


Figure 7 Geometry of Hexagonal Honeycomb Cell

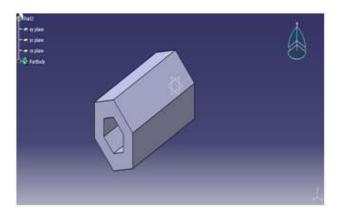


Figure 8 Modeling of Hexagonal Honeycomb Cell

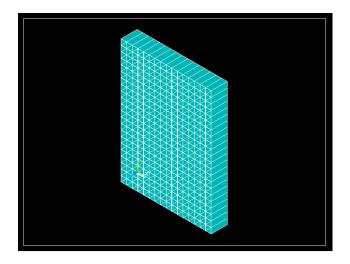


Figure 9 Pattern of Hexagonal Honeycomb Cells

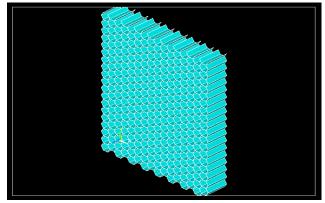


Figure 10 Assembly of Hexagonal Honeycomb cells with structure

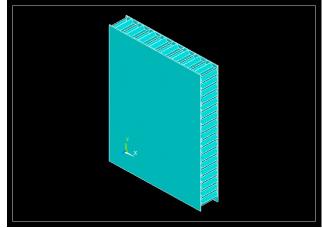


Figure 11 Geometry of Square Sandwich Cell

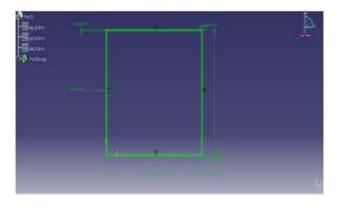


Figure 12 Modeling 3D- Square Honeycomb Cell

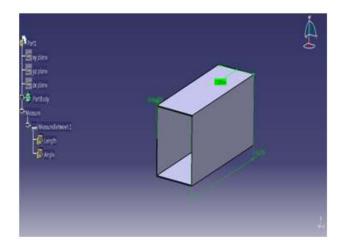


Figure 13 Assembly of square cell

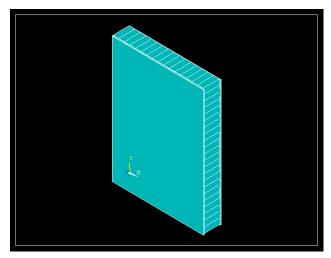


Figure 14 Assembly of square structure with panels

5. ANALYSIS OF HONEYCOMB SANDWICH STRUCTURE

Heat transfer analysis plays a very important role in the design of many engineering applications. Heat transfer analysis calculates the temperature distribution and related thermal quantities in the system or component .In general, the heat transfer in honeycomb sandwich panels is as a result of (1) conduction of heat in the cell walls, (2) radiation interchange within the cell, and (3) convection of heat through the air at the back side of the panel. However, this paper is concerned with sandwich panels in which the primary modes of heat transfer are due to conduction in the cell walls and radiation exchange within the cell. For most honeycomb cores used in the fabrication of sandwich panels, it can be shown that they heat exchange by convection and conduction within the air contained in the cell is negligible compared to conduction in the cell walls and radiation within the cell.

5.1 To simplify the analysis, the following assumptions are introduced.

First, honeycomb cells have the same effective density, but different geometrical shapes are considered (i.e., hexagon & square shapes).

Second, the effect of internal radiation turned out to be much smaller than that of conduction for the present TPS core geometry, hence radiation can be negligible.

Third, the thermal properties of the materials used do not change with the temperature.

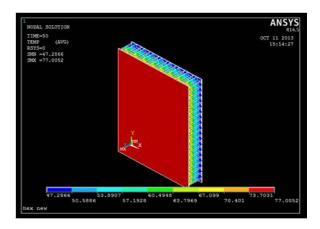
Fourth, there is no convection heat transfer inside the panel, as the experiment will take place inside a still environment. Convection heat transfer is considered for backside of the panel.

5.2 Heat Transfer Analysis

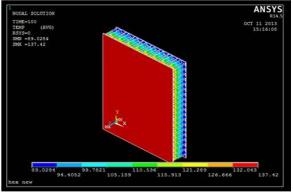
Heat transfer is a science that studies the energy transfer between two bodies due to temperature difference. Conductive heat transfer analysis on honeycomb sandwich panels and the tiny volume inside each honeycomb cell, convection heat transfer of the interior air mass were neglected. This section studies the effect of honeycomb cell geometry on the heat- insulating performance of the TPS panel. Before doing analysis to mesh the model so that the effectively find the change in temperature at each and every point. Perform heat transfer analysis under transient state condition.

5.3 Transient Thermal Analysis

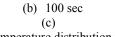
Transient Thermal Analysis determines temperatures and other thermal quantities that vary over time. Engineers commonly use temperatures that a transient thermal analysis calculates as input to structural analysis evaluations. A transient thermal analysis follows basically the same procedures as a steady –state thermal analysis. The main difference is that applied loads in a transient thermal analysis are functions of time. To specify time-dependent loads, use both the function t ool to define an equation or function describing the curve and then apply the function as a boundary condition or divide the load –versus –time load in to load steps. Shown in figures 15 (a) & (b) analysis of aluminium hexagonal honeycomb sandwich structure with different times. Figure 16 was plotted time vs temperature of bottom plate. Shown in figures 17 (a) & (b) analysis of aluminium hexagonal honeycomb sandwich structure with different times. Figure 18 was plotted time vs temperature of bottom plate.

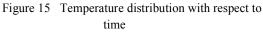


(a) 50 sec









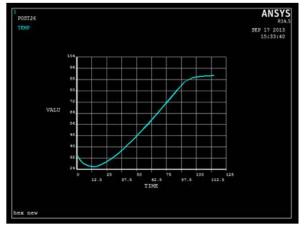
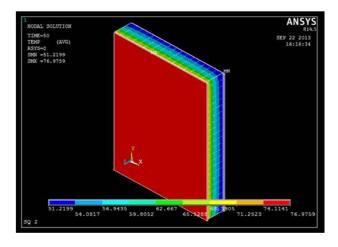
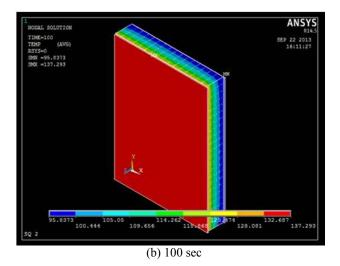


Figure 16 Time vs Temperature for bottom plate of aluminium hexagonal structure



(a) 50 sec





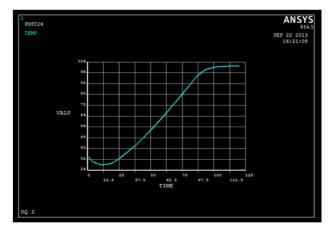


Figure 18 Time vs Temperature for bottom plate of aluminium square structure

6. EXPERIMENTAL TESTING

The honeycomb panel and core is mostly empty space. As such, when heat travels through the core, most of it is conducted through the thin walls of the cells, which have a very low area of conductance. This requires a large temperature difference between the two face sheets to move the heat through the core. Also, because of the empty space, radiation heat transfer is also a factor. Compared to conduction, radiation is a very poor way to move heat around, hence radiation can be neglected. How much heat can be shielded through the panel is a necessary piece of information when designing heat transfer analysis.

The purpose of this experiment is to determine a way to find the heat insulation performance of an aluminum honeycomb panel when heat is moving through it. The heat transfer analysis of honeycomb sandwich structure specimen at different temperatures was measured with respect to time.

6.1 Test Articles

The honeycomb panel test article was designed to simulate the local response near the middle of the lower wing honeycomb sandwich panel skin adjacent to the wheel well. The size of the hexagonal sandwich panel is 115×85 sq.mm and the height of the core is 15mm and the thickness of the top & bottom plate is 0.7mm. Face sheets are bonded with epoxy adhesive. Aluminum material temperature 150° C limits for usage in Aerospace. The IR (Infrared) lamps are used to heat the specimen plate. The rate of heating is controllable. The thermocouple records the temperature levels on the specimen. The rate of heating is chosen such that the limiting temperature is reached in the time of a couple of minutes, to simulate the aerospace flight environment at high speeds. A Schematic block diagram of the Experimental model is as shown in Figure 19

BLOCK DIAGRAM

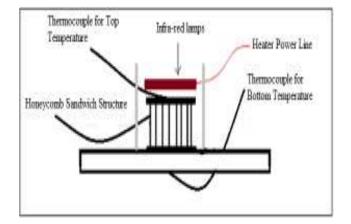


Figure 19 A Schematic of the Experimental Model

6.2 Experimental set -up

The aluminium honeycomb specimen was equipped with four temperature sensors. Two were placed on the upper skin, and two were placed symmetrically on the lower skin. The position of the thermocouples is indicated in Figure 20, with an order of magnitude for the specimen's dimensions. After the sensors were correctly attached, the heat supplied to the upper surface of the test specimen. The heat transfer was analyzed by measuring the temperature in the upper and lower (skin) plates using the thermocouples. Figure 21 shows a picture specimen before testing with thermocouples. It has insulation all the sides of insulations.



Figure 20 Pictures of the specimen before testing with thermocouples



Figure 21 Picture of the Specimen applied both sides Insulations

The specimen was placed near to infrared lamps, surrounded by zirconium fiber insulations; lower face of the specimen was exposed in air. According to Fourier's Law, The upper face sheet, honeycomb core and a lower face sheet of the sandwich structure can be treated as a series connection for heat transfer.



Figure 22 Infra-red lamps, close-up view

6.3 Infra-red lamp cluster

Infra-red lamps were used to generate a controlled temperature over the test specimen. The cluster is composed of a series of infra-red lamps aligned vertically, as depicted in Figure 22. The honeycomb sandwich panel was fixed on a support column, and then placed in front of the lamps. The lamp clusters heat energy emission was controlled such that it created a temperature gradient of 1.3° C/sec over the test specimen. During this experiment, a thermocouple was inserted in the middle of the aluminium honeycomb sandwich panel, and the luminance temperature of the hot surface was measured. The honeycomb sandwich structure is as shown in Figure 23.



Figure 23 Heating of Honeycomb sandwich panel

Various views of the insulated honeycomb sandwich structure is as shown in Figure 24. Aluminium honeycomb sandwich structure top plate and bottom plate experimental values are plotted in the graph. In this graph maximum temperature difference was 50.58° C at 86.36 seconds as shown in Figure 25.



Figure 24 Insulated Honeycomb sandwich Panel

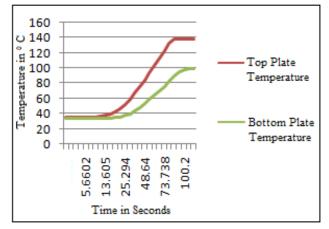


Figure 25 Experimental values for aluminium honeycomb sandwich structure

7. RESULTS AND DISCUSSION

The effect of honeycomb cell geometry on the heat-insulating performance of an aluminium alloy TPS has been analyzed. The results of heat-transfer, of aluminium alloy honeycomb TPS panels are presented in Table-2 and Table-3. Figure 26 and Figure 27 shows the difference between the top plate and the bottom plate temperatures, ΔT is a measure of the heat-insulating performance of the TPS. The larger the ΔT values of the better the heat-insulating performance. It was observed that hexagonal cell geometry reaches a maximum in 86.36 sec of 50.58°C and square cell geometry reaches a maximum of 87.13 seconds at 39.91°C then it decreases slightly with the increasing time, t. Aluminium hexagonal honeycomb structure for heat insulating is better than square honeycomb structure. The effect of internal radiation turned out to be much smaller than that of conduction for the present TPS core geometry.

	ТР	BP	Δt-	BP Temp- Evenori	Δt- Evpori
Time	Temp-	Temp- ANSYS	ANSYS	Experi mental	Experi mental
1	35.812	33.2091	2.6029	33.415	2.397
5.6602	35.586	28.2062	7.3798	33.64	1.946
11.59	35.779	26.1249	9.6541	33.672	2.107
15.619	37.969	25.9457	12.0233	33.93	4.039
20.876	42.188	27.3743	14.8137	34.22	7.968
25.294	46.536	29.5047	17.0313	35.154	11.382
30.702	52.204	32.7359	19.4681	36.893	15.311
36.514	58.807	36.6954	22.1116	39.566	19.241
42.573	66.794	41.3665	25.4275	43.237	23.557
48.64	74.974	46.4584	28.5156	47.584	27.39
54.834	83.831	51.9596	31.8714	52.705	31.126
61.115	93.074	57.793	35.281	58.34	34.734
67.431	102.864	63.9321	38.9319	63.751	39.113
73.738	112.43	70.1085	42.3215	69.386	43.044
80.045	122.575	76.5323	46.0427	75.473	47.102
86.36	132.623	82.9658	49.6572	82.042	50.581
92.827	137	87.6827	49.3173	88.386	48.614
100.2	137.473	89.837	47.636	94.57	42.903
114.96	137.61	90.9112	46.6988	98.251	39.359

Table- 2. Aluminium-Hexagonal Honeycomb Sandwich Structure

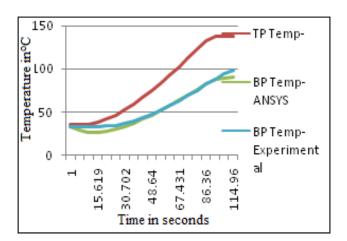
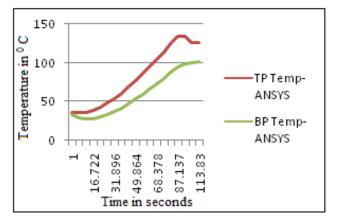
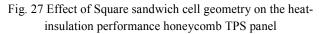


Figure 26 Effect of hexagonal honeycomb cell geometry on the heat-insulation performance of honeycomb TPS panel

	TP Temp-	BP Temp-		
Time	ANSYS	ANSYS	Δt - ANSYS	
1	35.812	33.4527	2.3593	
5.23	35.812	29.601	6.211	
10.155	35.554	28.1201	7.4339	
16.722	38.807	28.2581	10.5489	
21.546	42.704	30.35	12.354	
26.133	47.277	33.2375	14.0395	
31.896	53.525	37.3995	16.1255	
37.831	60.417	42.182	18.235	
43.839	68.404	47.5543	20.8497	
49.864	76.81	53.3542	23.4558	
55.982	85.409	59.5411	25.8679	
62.175	94.845	66.0926	28.7524	
68.378	104.507	72.8776	31.6294	
74.616	113.686	79.7245	33.9615	
80.95	123.927	87.0121	36.9149	
87.137	133.879	93.9651	39.9139	
93.323	133.814	98.4125	35.4015	
100.16	125.473	100.202	25.271	
113.83	125.854	101.004	20.538	

Table- 3 Aluminium-Square Honeycomb Sandwich Structure





6.1 Comparison between right, hexagonal structure and square structure

When the heat insulating performance of the honeycomb sandwich panels has been reasonably well-known, good agreement has been obtained between ANSYS and Experimental results. Some success has been attained in determining uncertain structural characteristics by attempting to match ANSYS and experimental results. For the most part, effort has been concentrated on determining the temperature variation of right, hexagonal panel and square panel with respect to time. Table-4 shows a comparison of ANYSIS and experimental results for the temperature difference. Aluminum hexagonal honeycomb structure for heat insulating is better than square honeycomb structure

S	Cell type	Material	Time in	Maximum Δt Values	
No			sec	(max. heat shield)	
				Experimen	ANSYS
				tal	
1	Right Hexagona 1	Aluminum- 2024	86.36	50.581	49.6572
2	Square	Aluminum- 2024	87.137		39.9139

Table- 4 Heat Insulating performance of TPS honeycombpanel with different cell geometry

8. CONCLUSION

The geometrical (shape) analysis of different candidate honeycomb cells that have the same effective density but different cell geometrical shapes. Heat-transfer, analysis are performed on a aluminium alloy thermal protection system (TPS) for future vehicles. Effect of honeycomb cell geometry on the heat-insulating performance, has been found. Infra-red experiment was conducted to investigate the response of several areas of the shield during the flight. The Aluminium alloy specimen researches its temperature limits in 90 seconds. (After 90 seconds the temperature is reached for study state condition) For aerospace use, it is desirable to use the material which can attain its temperature limit after the elapse of longer time. The heat-insulating performance of a honeycomb TPS is insensitive to the shape of the honeycomb cell under the same effective core density.

REFERENCES

- [1] Thermostructural Analysis of Honeycomb Sandwich Panels, K.Kantha Rao, K. Jayathirtha Rao, *International Journal of EngineeringScience&Advanced Technology*, volume-2, issue-5 Sep-Oct2012.
- [2] Strength Analysis on Honeycomb Sandwich Panels of different Materials K.Kantha Rao, K. Jayathirtha Rao, A.G.Sarwade, M.Sarath Chandra, *International Journal of engineering research and applications* volume 2, issue 3, May-Jun 2012,
- [3] Shigenori Kabashima & Tsuyoshi Ozaki, Numerical Approach to calculate thermal expansion of Honeycomb sandwich panel with composite face sheets, *Advanced Composite Materials*, Apr 2012.
- [4] J. Fatemi Dutch Space, 2303 DB Leiden, The Netherlands and M. H. J. Lemmen Effective Thermal/Mechanical Properties of Honeycomb Core Panels for Hot Structure Applications, *Journal of Spacecraft and rockets* vol. 46, No. 3, May–June 2009

- [5] P. Innocenti and F. Scarpa Thermal Conductivity Properties and Heat Transfer Analysis of Multi-reentrant Auxetic Honeycomb Structures, *Journal of Composite Materials* 2009 43: 2419, August 2009
- [6] Thermostructural Behavior of a Hypersonic Aircraft Sandwich Panel Subjected to Heating on One Side William L. Ko Dryden Flight Research Center Edwards, *California NASA Technical Memorandum* 4769, April 1997
- [7] NASA Langley Research Center, Hampton, VA 23681, Ceramic Matrix Composite (CMC) Thermal Protection Systems (TPS) and Hot Structures for Hypersonic Vehicles1 David E. Glass2, March 2007
- [8] Comparison of Thermo-Structural Responses for Integrated Thermal Potection Panels with different Corrugated Core Configurations, Shu-Yuan Zhao, Jian-Junli, Xiao-Dong He, Journal of Harbin Institute of Technology (New Series), Vol.20, No.6,2013
- [9] Analysis and Sizing for Transient Thermal Heating of Insulated Aerospace Vehicle Structures, *Max L. Blosser Langley Research Center, Hampton, Virg,* August 2012, NASA/TP–2012-217595
- [10] P. Innocenti and F. Scarpa Thermal Conductivity Properties and Heat Transfer Analysis of Multi-reentrant Auxetic Honeycomb Structures, *Journal of Composite Materials* 2009 43: 2419, August 2009
- [11] Hazem E. Soliman, Dhaval P. Makhecha, Summit Vasudeva, Rakesh K. Kapania and Owen Hughes, On the Static Analysis of Sandwich Panels with Square Honeycomb Core by the *American Institute of Aeronautics and Astronautics*, May 2006
- [12] Investigation on the square cell honeycomb structures under axial loading, Sen Liang *, H.L. Chen, *Composite Structures* 72 (2006) 446–454
- [13] Research progress on thermal protection materials and structures of hypersonic vehicles, YANG Ya-zheng, YANG Jia-ling,FANG *Dai-ning*, *Appl. Math. Mech.* -*Engl. Ed.*, 2008, **29**(1):51–60
- [14] Improved lumped models for transient combined convective and radiative cooling of multi-layer composite slabs Chen An, Jian Su *Applied Thermal Engineering* 31 (2011) 2508e2517
- [15] MDA of Hexagonal Honeycomb Plates used for Space Applications, A.Boudjemai , M.H. Bouanane, Mankour, R. Amri, H. Salem, B. Chouchaoui, World Academy of Science, Engineering and Technology 66 2012

[16] *TALAT Lecture 1501*, Aluminium: Physical Properties, Characteristics and Alloys, prepared by Ron Cobden, Alcan, Banbury

 [17] Thermal Buckling of Metal Foam Sandwich Panels for Convective Thermal Protection Systems Joseph F. Rakow and Anthony M. Waas, *Journal Of Spacecraft And Rockets*, Vol. 42, No. 5, September–October 2005

- [18] On the Static Analysis of Sandwich Panels with Square Honeycomb Core, Hazem E. Soliman*, Dhaval P. Makhecha, Summit Vasudeva, Rakesh
- K. Kapania and Owen Hughes, 47th AIAA/ASME/ASCE/AHS/ASC Structures, Structural Dynamics, and Materials Con. 1-4 May 2006, Newport, Rhode Island